



500MHz, Low-Power, Current-Mode Feedback Amplifiers

MAX4112/MAX4113

General Description

The MAX4112/MAX4113 current-mode feedback amplifiers combine high-speed performance with low-power operation. The MAX4112 is optimized for closed-loop gains of 2V/V or greater, while the MAX4113 is optimized for gains of 8V/V or greater.

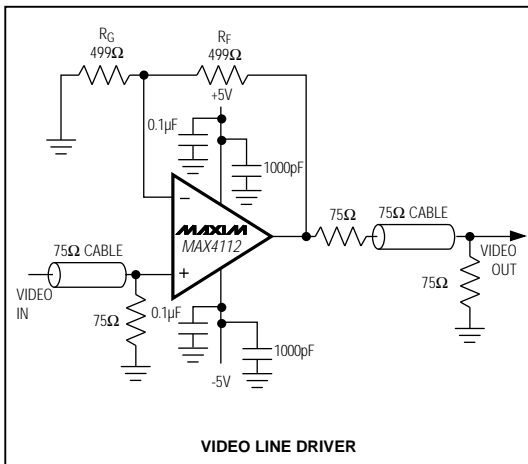
The MAX4112/MAX4113 require only 5mA of supply current and deliver bandwidths of 500MHz ($A_v \geq 2V/V$) and 275MHz ($A_v \geq 8V/V$), respectively. The high slew rates (1200V/ μ s and 1800V/ μ s) provide exceptional full-power bandwidths (300MHz and 250MHz), making these amplifiers ideal for high-performance pulse and RGB video applications.

These high-speed op amps have a wide output voltage swing of $\pm 3.5V$ into 100 Ω and a high current-drive capability of 80mA.

Applications

- Broadcast and High-Definition TV Systems
- RGB Video
- Pulse/RF Amplifier
- Ultrasound
- Active Filters
- ADC Buffers

Typical Application Circuit



Features

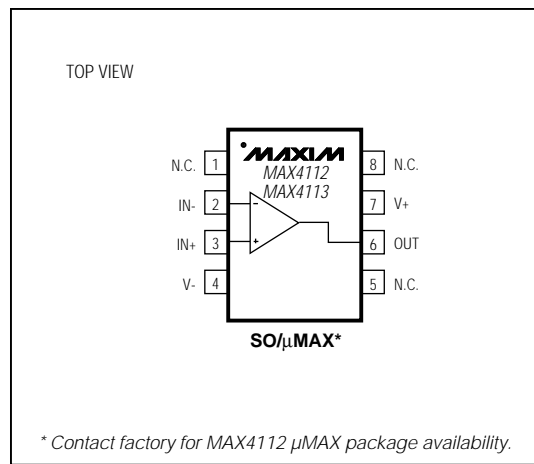
- ◆ 500MHz -3dB Bandwidth (MAX4112)
275MHz -3dB Bandwidth (MAX4113)
- ◆ 0.1dB Gain Flatness to 30MHz (MAX4112)
- ◆ 1200V/ μ s Slew Rate (MAX4112)
1800V/ μ s Slew Rate (MAX4113)
- ◆ 300MHz Full-Power Bandwidth ($V_o = 2V_p-p$, MAX4112)
250MHz Full-Power Bandwidth ($V_o = 2V_p-p$, MAX4113)
- ◆ High Output Drive: 80mA
- ◆ Low Power: 5mA Supply Current

Ordering Information

PART	TEMP. RANGE	PIN-PACKAGE
MAX4112ESA	-40°C to +85°C	8 SO
MAX4112EUA	-40°C to +85°C	8 μ MAX*
MAX4113ESA	-40°C to +85°C	8 SO

* Contact factory for μ MAX package availability.

Pin Configuration



* Contact factory for MAX4112 μ MAX package availability.



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ABSOLUTE MAXIMUM RATINGS

Power Supply Voltage (V_{CC} to V_{EE}) 12V
 Voltage on Any Pin to Ground or Any Other Pin V_{CC} to V_{EE}
 Short-Circuit Duration (V_{OUT} to GND)
 $V_{IN} < 1.5V$ Continuous
 $V_{IN} > 1.5V$ 0sec
 Continuous Power Dissipation ($T_A = +70^\circ C$)
 SO (derate 5.88mW/C above $+70^\circ C$) 471mW
 μ MAX (derate 4.10mW/C above $+70^\circ C$) 330mW

Operating Temperature Range
 MAX4112E_A/MAX4113E_A $-40^\circ C$ to $+85^\circ C$
 Storage Temperature Range $-65^\circ C$ to $+160^\circ C$
 Lead Temperature (soldering, 10sec) $+300^\circ C$

Stresses beyond those listed under "Absolute Maximum Ratings" may cause permanent damage to the device. These are stress ratings only, and functional operation of the device at these or any other conditions beyond those indicated in the operational sections of the specifications is not implied. Exposure to absolute maximum rating conditions for extended periods may affect device reliability.

ELECTRICAL CHARACTERISTICS

($V_{CC} = 5V$, $V_{EE} = -5V$, $T_A = T_{MIN}$ to T_{MAX} , typical values are at $T_A = +25^\circ C$, unless otherwise noted.)

PARAMETER	SYMBOL	CONDITIONS	MIN	TYP	MAX	UNITS
DC SPECIFICATIONS						
Input Offset Voltage	V_{OS}	$V_{OUT} = 0V$		1	8	mV
Input Offset Voltage Drift	TCV_{OS}	$V_{OUT} = 0V$		10		$\mu V/^\circ C$
Positive Input Bias Current	I_{B+}	$V_{OUT} = 0V$, $V_{IN} = -V_{OS}$		3.5	20	μA
Negative Input Bias Current	I_{B-}	$V_{OUT} = 0V$, $V_{IN} = -V_{OS}$		3.5	20	μA
Input Resistance		IN+		500		$k\Omega$
		IN-		30		Ω
Input Capacitance		IN+		2		pF
Input Voltage Noise	e_n	$f = 10kHz$		2.2		nV/\sqrt{Hz}
Integrated Voltage Noise	E_{nRMS}	$f = 1MHz$ to $100MHz$		27		μV_{RMS}
Positive Input Current Noise	i_{n+}	$f = 10kHz$	MAX4112	13		pA/\sqrt{Hz}
			MAX4113	9		
Negative Input Current Noise	i_{n-}	$f = 10kHz$		14		pA/\sqrt{Hz}
Common-Mode Input Voltage	V_{CM}		-2.5		2.5	V
Common-Mode Rejection	CMR	$V_{CM} = \pm 2.5V$		45	50	dB
Power-Supply Rejection	PSR	$V_S = \pm 4.5V$ to $\pm 5.5V$		60	80	dB
Open-Loop Transimpedance	Z_{OL}	$V_{OUT} = \pm 2.0V$, $V_{CM} = 0V$, $R_L = 100\Omega$	250	500		$k\Omega$
Quiescent Supply Current	I_{SY}	$V_{IN} = 0V$		5	6.5	mA
Output Voltage Swing	V_{OUT}	$R_L = \infty$	± 3.5	± 3.8		V
		$R_L = 100\Omega$	± 3.1	± 3.5		
Output Current Drive	I_{OUT}	$R_L = 30\Omega$, $T_A = 0^\circ C$ to $+85^\circ C$	65	80		mA

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ELECTRICAL CHARACTERISTICS (continued)

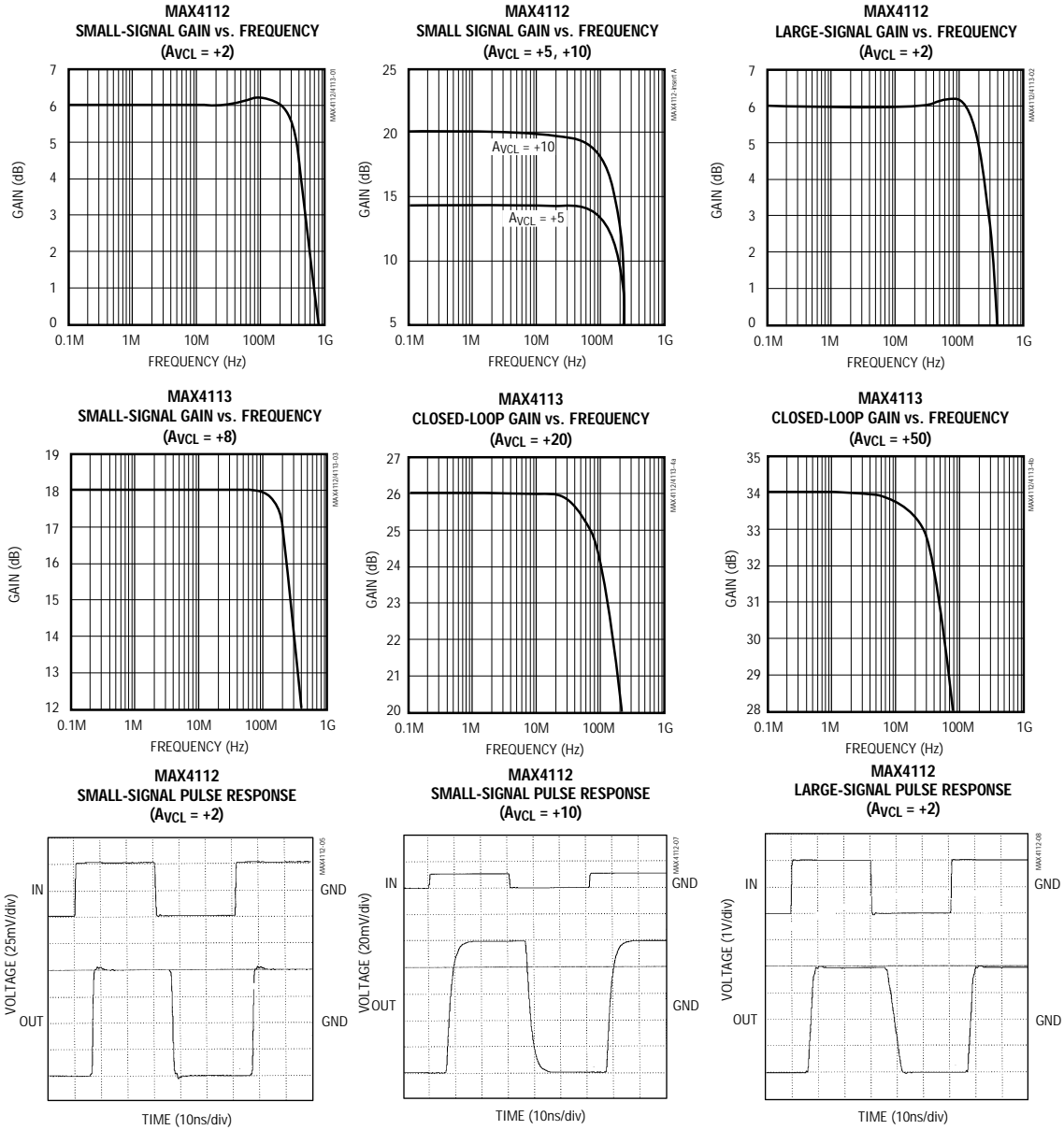
($V_{CC} = 5V$, $V_{EE} = -5V$, $T_A = T_{MIN}$ to T_{MAX} , typical values are at $T_A = +25^\circ C$, unless otherwise noted.)

PARAMETER	SYMBOL	CONDITIONS	MIN	TYP	MAX	UNITS
AC SPECIFICATIONS						
-3dB Bandwidth	BW _{-3dB}	$V_{OUT} \leq 0.1V_{RMS}$	MAX4112	500		MHz
			MAX4113	275		
0.1dB Bandwidth	BW _{0.1dB}	MAX4112, $A_{VCL} = +2$		30		MHz
		MAX4113, $A_{VCL} = +8$		90		
Full-Power Bandwidth	FPBW	$V_O = 2V_{p-p}$	MAX4112	300		MHz
			MAX4113	250		
Slew Rate	SR	$-2V \leq V_{OUT} \leq 2V$	MAX4112	1200		V/ μs
			MAX4113	1800		
Settling Time	t_s	to 0.1%, $-1V \leq V_{OUT} \leq 1V$, $R_L = 100\Omega$	MAX4112	15		ns
			MAX4113	10		
		to 0.01%, $-1V \leq V_{OUT} \leq 1V$, $R_L = 100\Omega$	MAX4112	35		
			MAX4113	25		
Rise/Fall Times	t_r, t_f	10% to 90%, $-2V \leq V_{OUT} \leq 2V$, $R_L = 100\Omega$		3		ns
		10% to 90%, $-50mV \leq V_{OUT} \leq 50mV$, $R_L = 100\Omega$		0.8		
Differential Gain	DG	$f = 3.58MHz$	MAX4112, $A_{VCL} = +2$	0.02		%
			MAX4113, $A_{VCL} = +8$	0.02		
Differential Phase	DP	$f = 3.58MHz$	MAX4112, $A_{VCL} = +2$	0.03		degrees
			MAX4113, $A_{VCL} = +8$	0.04		
Input Capacitance	C_{IN}			2		pF
Output Impedance	Z_{OUT}	$f = 10MHz$, $A_{VCL} = +2$		0.9		Ω
Spurious-Free Dynamic Range	SFDR	$f_C = 5MHz$, $V_{OUT} = 2V_{p-p}$	MAX4112, $A_{VCL} = +2$	-68		dBc
			MAX4113, $A_{VCL} = +8$	-62		
Two-Tone Third-Order Intercept	IP3	$f_C = 10MHz$, $A_{VCL} = +2$		36		dB

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Typical Operating Characteristics

(V_{CC} = 5V, V_{EE} = -5V, R_F = 499Ω, R_L = 100Ω, T_A = +25°C, unless otherwise noted.)

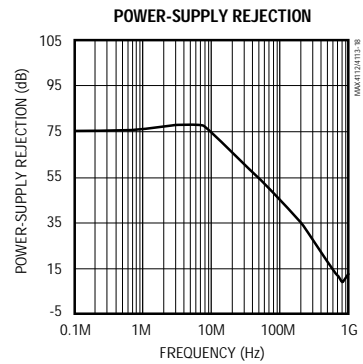
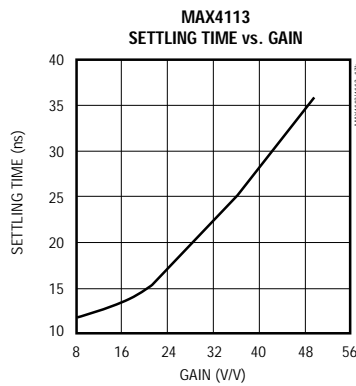
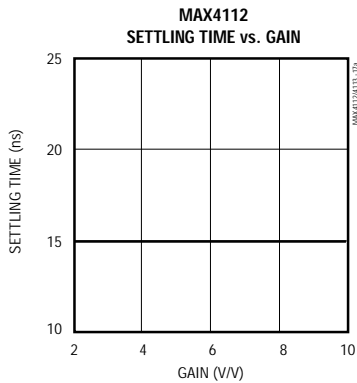
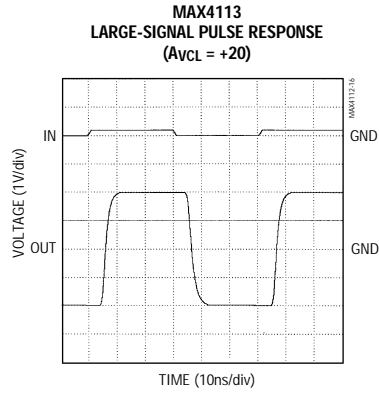
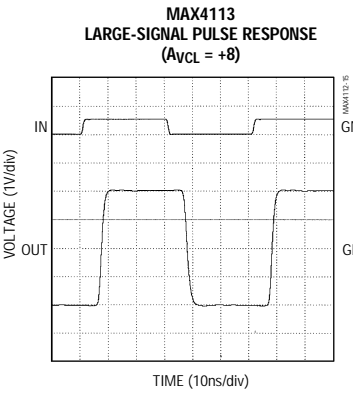
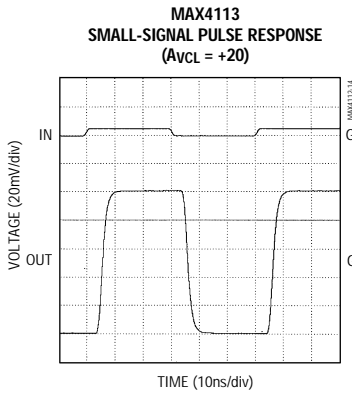
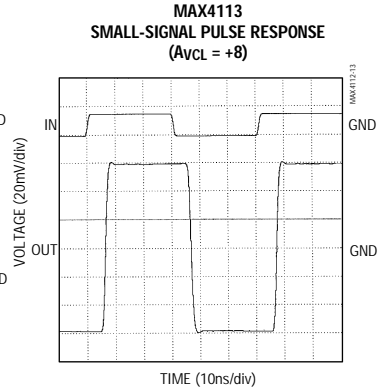
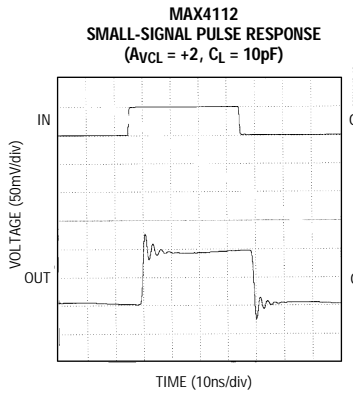
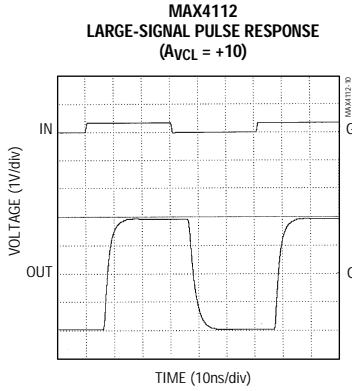


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Typical Operating Characteristics (continued)

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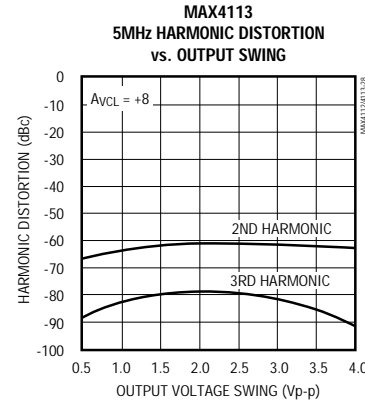
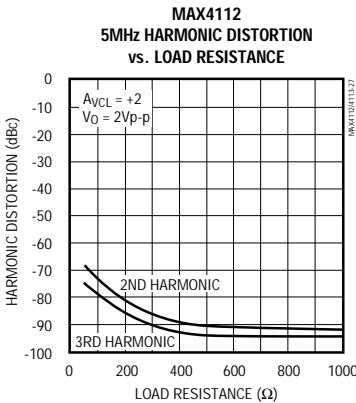
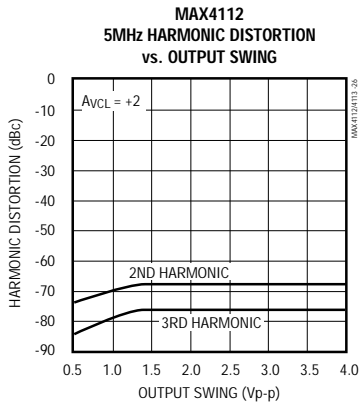
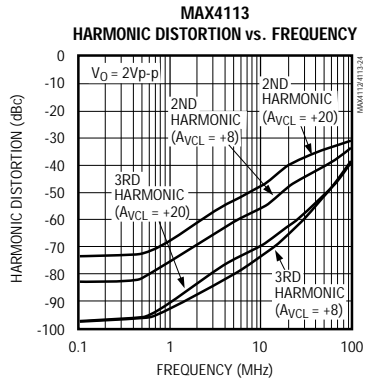
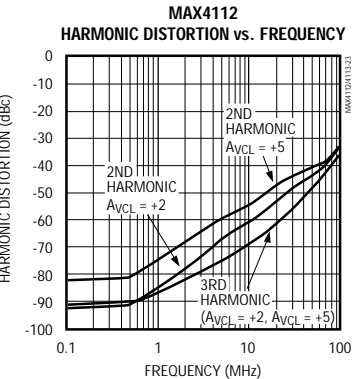
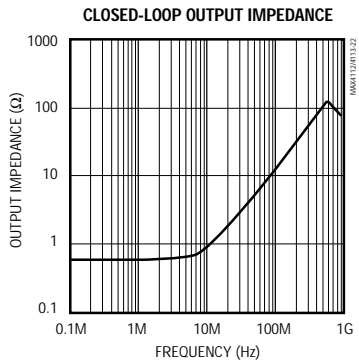
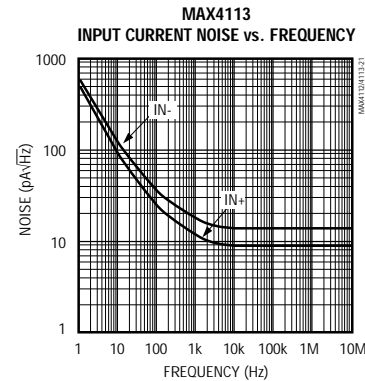
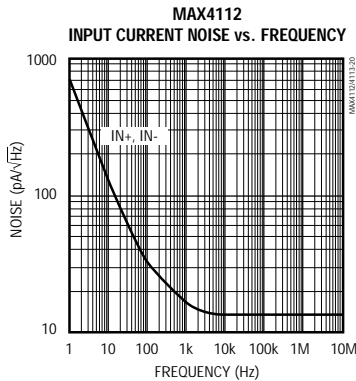
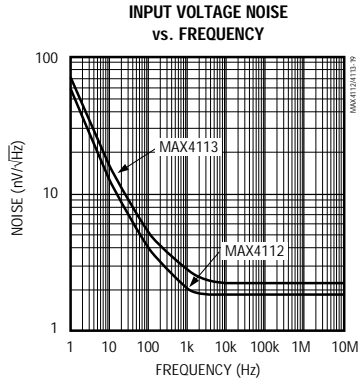
MAX4112/MAX4113



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Typical Operating Characteristics (continued)

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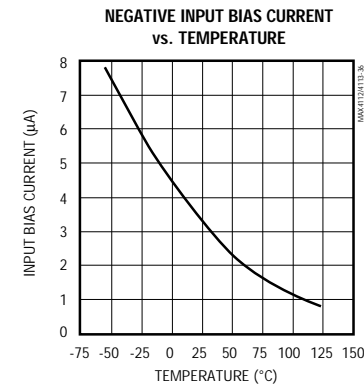
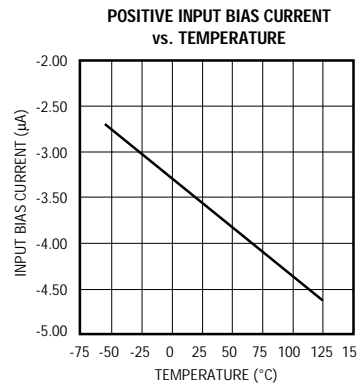
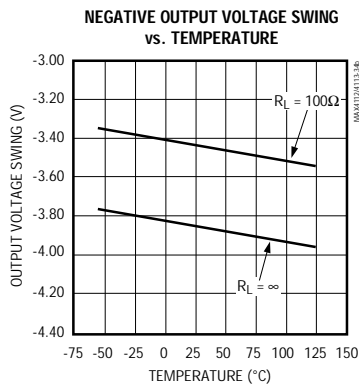
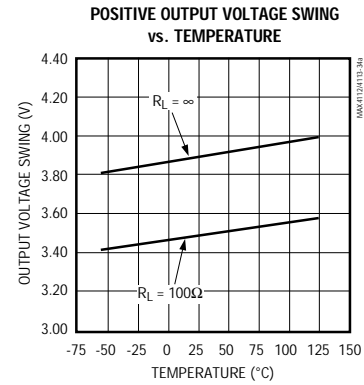
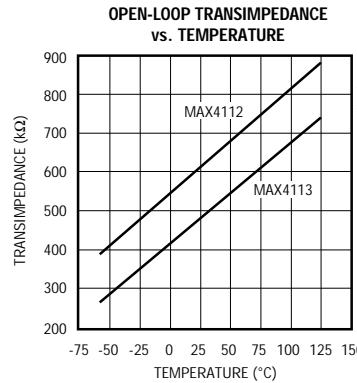
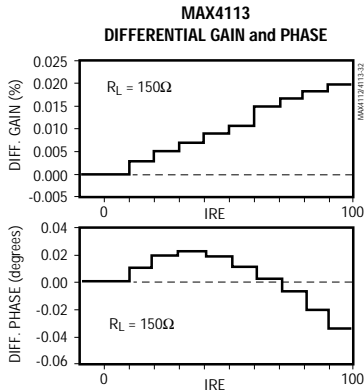
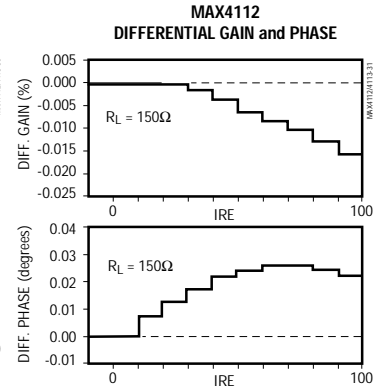
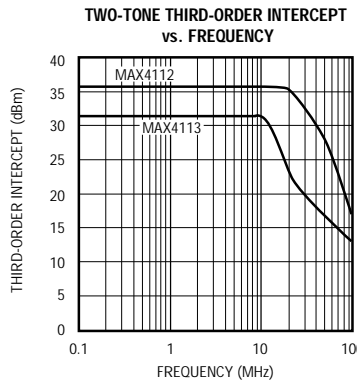
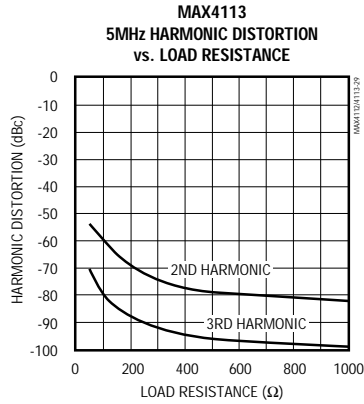


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Typical Operating Characteristics (continued)

($V_{CC} = 5V$, $V_{EE} = -5V$, $R_F = 499\Omega$, $R_L = 100\Omega$, $T_A = +25^\circ C$, unless otherwise noted.)

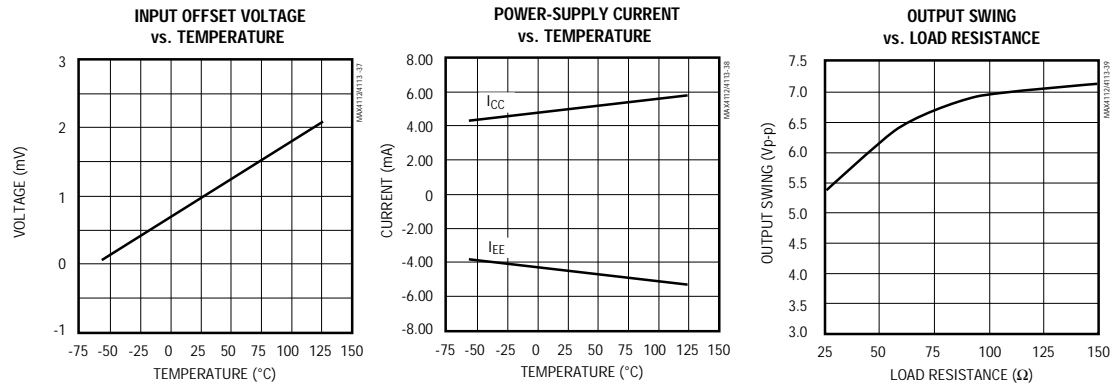
MAX4112/MAX4113



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Typical Operating Characteristics (continued)

(V_{CC} = 5V, V_{EE} = -5V, R_F = 499Ω, R_L = 100Ω, T_A = +25°C, unless otherwise noted.)



Pin Description

PIN	NAME	FUNCTION
1, 5, 8	N.C.	No Connection, not internally connected
2	IN-	Inverting Input
3	IN+	Noninverting Input
4	V _{EE}	Negative Power Supply, connect to -5V
6	OUT	Amplifier Output
7	V _{CC}	Positive Power Supply, connect to +5V

Detailed Description

The MAX4112 is optimized for closed-loop gains (A_{VCL}) of 2V/V or greater, while the MAX4113 is optimized for closed-loop gains of 8V/V or greater. These low-power, high-speed current-mode feedback amplifiers operate from ±5V supplies. They are designed to drive video loads with excellent distortion characteristics. The MAX4112's differential gain and phase are 0.02% and 0.03°, respectively; the MAX4113 exhibits gain/phase error specifications of 0.02% and 0.04°, respectively. These characteristics, plus a wide 0.1dB bandwidth, make the MAX4112/MAX4113 ideal for use in broadcast and graphics video systems. The combination of ultra-high speed and low power makes these parts ideal for use in general-purpose high-speed applications, such as medical imaging, industrial instrumentation, and communications systems.

Applications Information

Theory of Operation

Since the MAX4112/MAX4113 are current-feedback amplifiers, their open-loop transfer function is expressed as a transimpedance, ΔV_{OUT}/ΔI_{IN}, or Z_{OL}. The frequency behavior of the open-loop transimpedance is similar to the open-loop gain of a voltage-mode feedback amplifier. That is, it has a large DC value and decreases at approximately 6dB/octave.

Analyzing the follower with gain, as shown in Figure 1, yields the following transfer function:

$$\frac{V_{OUT}}{V_{IN}} = G \times \frac{Z_{OL}(s)}{Z_{OL}(s) + G \times R_{IN} + R_F}$$

where $G = A_{VCL} = 1 + R_F / R_G$, and $R_{IN} = 1 / g_M \cong 30\Omega$.

At low gains, $G \times R_{IN} \ll R_F$. Therefore, the closed-loop bandwidth is essentially independent of closed-loop gain. Similarly $Z_{OL} \gg R_F$ at low frequencies, so that:

$$\frac{V_{OUT}}{V_{IN}} = G = 1 + R_F / R_G$$

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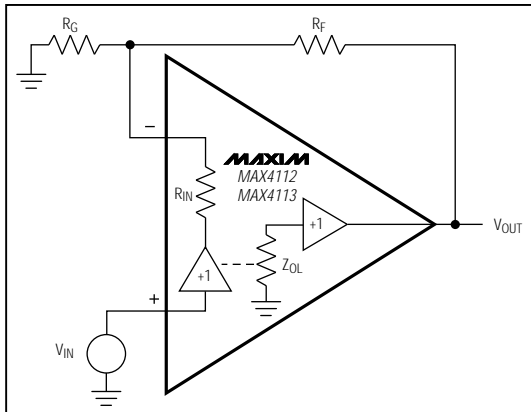


Figure 1. Current Feedback Amplifier

Layout and Power-Supply Bypassing

The MAX4112/MAX4113 have an RF bandwidth and, consequently, require careful board layout, including the possible use of constant-impedance Microstrip or Stripline techniques.

To realize the full AC performance of these high-speed amplifiers, pay careful attention to power-supply bypassing and board layout. The PC board should have at least two layers: a signal and power layer on one side, and a large, low-impedance ground plane on the other side. The ground plane should be as free of voids as possible. With multilayer boards, locate the ground plane on a layer that incorporates no signal or power traces.

Regardless of whether a constant-impedance board is used, it is best to observe the following guidelines when designing the board. Wire-wrap boards are much too inductive, and breadboards are much too capacitive; neither should be used. IC sockets increase para-

sitic capacitance and inductance, and should not be used. In general, surface-mount components give better high-frequency performance than through-hole components. They have shorter leads and lower parasitic reactances. Keep lines as short and as straight as possible. Do not make 90° turns; round all corners.

Observe high-frequency bypassing techniques to maintain the amplifier's accuracy. The bypass capacitors should include a 1000pF ceramic capacitor between each supply pin and the ground plane, located as close to the package as possible. Next, place a 0.01μF to 0.1μF ceramic capacitor in parallel with each 1000pF capacitor, and as close to them as possible. Then place a 10μF to 15μF low-ESR tantalum at the point of entry (to the PC board) of the power-supply pins. The power-supply trace should lead directly from the tantalum capacitor to the V_{CC} and V_{EE} pins. To minimize parasitic inductance, keep PC traces short and use surface-mount components.

Choosing Feedback and Gain Resistors

The MAX4112/MAX4113 are current-feedback amplifiers optimized for a 499Ω feedback resistor. Although a standard 5% value is sufficient, a 1% value is preferred to maintain consistency over a wide range of production lots. Changing feedback resistor value will reduce the bandwidth or cause excessive peaking. To change the magnitude of the gain, use the input resistor (R_F). Figure 2 shows the standard inverting and non-inverting configurations. Notice that the gain of the noninverting circuit (Figure 2a) is 1 plus the magnitude of the inverting closed-loop gain. Otherwise the two circuits are identical and equivalent (see Table 1).

DC and Noise Errors

There are several major error sources to consider in any operational amplifier. These apply equally to the MAX4112/MAX4113. Offset-error terms are given by the equation below. Voltage and current noise errors are

Table 1. Recommended Component Values

COMPONENT	MAX4112				MAX4113				
	-2	+2	+10	+25	-8	+8	+10	+50	+100
R _F (Ω)	499	499	499	499	499	499	499	499	499
R _G (Ω)	247	499	56	20	62.5	69	56	10	5
R _O (Ω)	49.9	49.9	49.9	49.9	49.9	49.9	49.9	49.9	49.9
R _S (Ω)	0	—	—	—	—	0	—	—	—
R _T (Ω)	62.5	49.9	49.9	49.9	250	49.9	49.9	49.9	49.9
Small-Signal Bandwidth (MHz)	180	500	100	50	325	275	235	50	23
0.1dB Flatness (MHz)	40	30	15	8	90	90	79	8	4

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root-square summed and, therefore, computed separately. In Figure 3, the total output offset voltage is determined by:

- a) The input offset voltage (V_{OS}) times the closed-loop gain ($1 + R_F / R_G$)
- b) The positive input bias current (I_{B+}) times the source resistor (R_S) (usually 50Ω or 75Ω), plus the negative input bias current (I_{B-}), times the parallel combination of R_G and R_F . In current-mode feedback amplifiers, the input bias currents may flow into or out of the device; for this reason, there is no benefit to matching the resistance at both inputs.

The equation for total DC error is:

$$V_{OUT} = \left[(I_{B+})R_S + (I_{B-})(R_F \parallel R_G) + V_{OS} \right] \left(1 + \frac{R_F}{R_G} \right)$$

- c) The total output referred noise voltage is:

$$e_{n(OUT)} = \left(1 + \frac{R_F}{R_G} \right) \sqrt{[(i_{n+})R_S]^2 + [(i_{n-})R_F \parallel R_G]^2 + (e_n)^2}$$

The MAX4112 has a very low, $2nV/\sqrt{Hz}$ noise voltage. The current noise at the positive input (i_{n+}) is $13pA/\sqrt{Hz}$, and the current noise at the inverting input is $14pA/\sqrt{Hz}$.

An example of the DC error calculations, using the MAX4112 typical data and the typical operating circuit using $R_F = R_G = 500\Omega$ ($R_F \parallel R_G = 250\Omega$) and $R_S = 50\Omega$ gives:

$$V_{OUT} = (3.5 \times 10^{-6} \times 50 + 3.5 \times 10^{-6} \times 250 + 10^{-3}) (1 + 1)$$

$$V_{OUT} = 4.1mV$$

Calculating total output noise in a similar manner yields:

$$e_{n(OUT)} = (1+1) \sqrt{(13 \times 10^{-12} \times 50)^2 + (14 \times 10^{-12} \times 250)^2 + (2 \times 10^{-9})^2}$$

$$e_{n(OUT)} = 4nV/\sqrt{Hz}$$

With a 200MHz system bandwidth, this calculates to $56.6\mu V_{RMS}$ (approximately $340\mu V_{p-p}$, choosing the six-sigma value).

Resistor Types

Surface-mount resistors are the best choice for high-frequency circuits. They are of similar material to metal-film resistors, but are deposited using a thick-film process in a flat, linear manner that minimizes inductance. Their small size and lack of leads also minimizes parasitic inductance and capacitance, yielding more predictable performance.

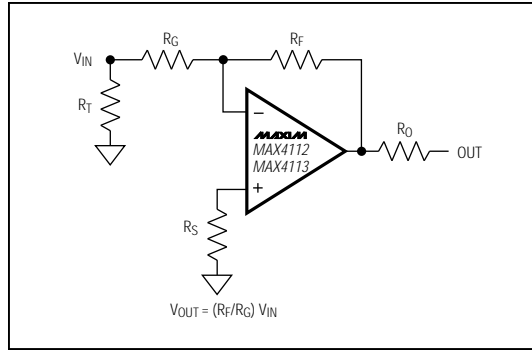


Figure 2a. Inverting Gain Configuration

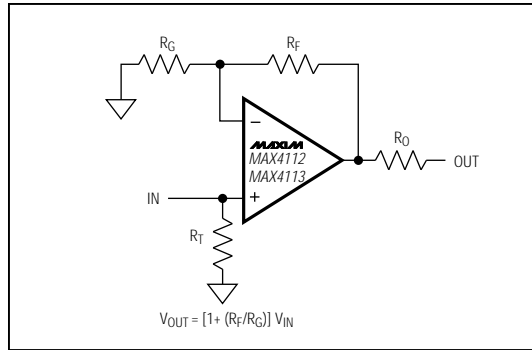


Figure 2b. Noninverting Gain Configuration

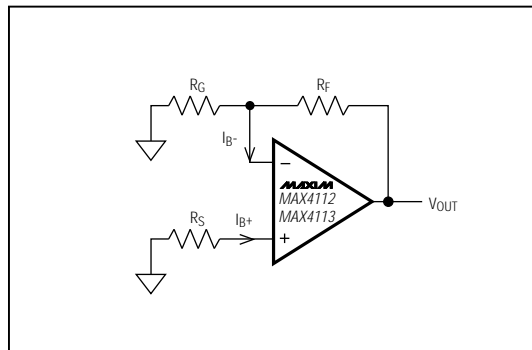


Figure 3. Output Offset Voltage

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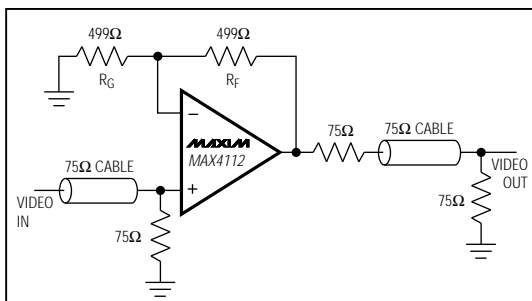


Figure 4. Video Line Driver

Metal-film resistors with leads are manufactured using a thin-film process where resistive material is deposited in a spiral layer around a ceramic rod. Although the materials used are noninductive, the spiral winding presents a small inductance (about 5nH) that may have an adverse effect on high-frequency circuits.

Carbon composition resistors with leads are manufactured by pouring the resistor material into a mold. This process yields relatively low-inductance resistors that are very useful in high-frequency applications, although they tend to cost more and have more thermal noise than other types. The ability of carbon composition resistors to self-heal after a large current overload makes them useful in high-power RF applications.

For general-purpose use, surface-mount metal-film resistors seem to have the best overall performance for low cost, low inductance, and low noise.

Video Line Driver

The MAX4112/MAX4113 are optimized (gain flatness) to drive coaxial transmission lines when the cable is terminated at both ends, as shown in Figure 4. Cable frequency response may cause variations in the flatness of the signal.

Driving Capacitive Loads

The MAX4112/MAX4113 are optimized for AC performance. They are not designed to drive highly capacitive loads. Reactive loads will decrease phase margin and may produce excessive ringing and oscillation. Figure 5 shows a circuit that eliminates this problem. The small (usually 5Ω to 20Ω) isolation resistor, R_S , placed before the reactive load will prevent ringing and oscillation. At higher capacitive loads, AC performance will be controlled by the interaction of the load capacitance and isolation resistor.

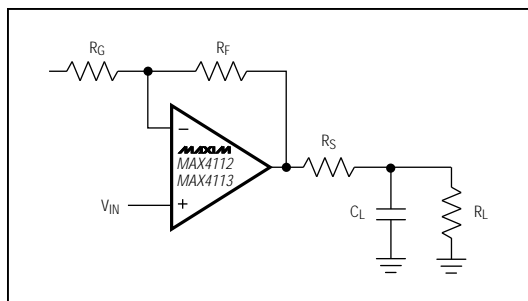


Figure 5a. Using an Isolation Resistor (R_S) for High Capacitive Loads

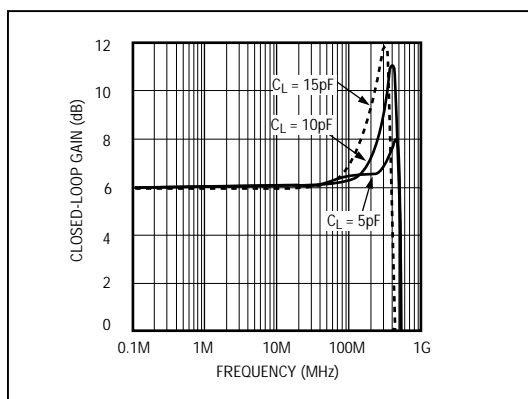


Figure 5b. Frequency Response vs. Capacitive Load—No Isolation Resistor

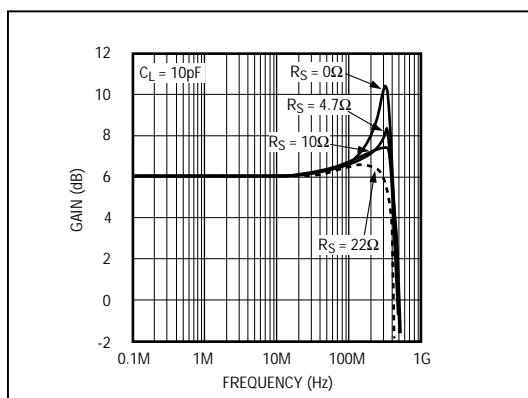


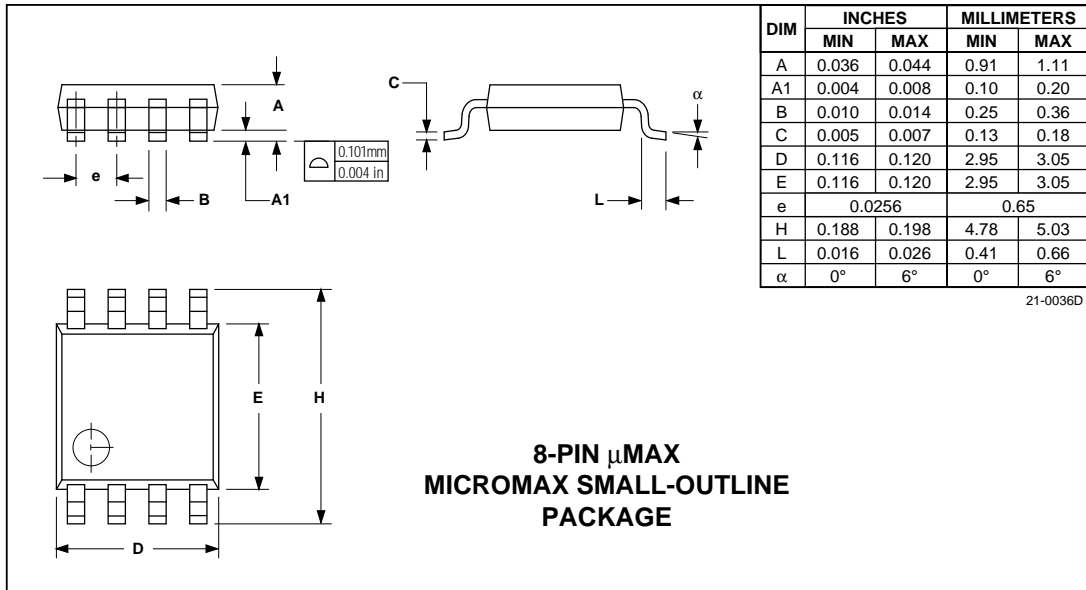
Figure 5c. Frequency Response vs. Isolation Resistance (see Figure 5a for circuit)

500MHz, Low-Power, Current-Mode Feedback Amplifiers

Chip Information

TRANSISTOR COUNT: 53

Package Information



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